

## Simulation of a clamping ring under high dynamic loading

S. Edelmann / C. Gross / <u>H. Chladek</u> INPROSIM GmbH © 2009

## 7<sup>th</sup> European LS-DYNA Conference

14th - 15th May 2009, Salzburg, Austria



14th - 15th May 2009, Salzburg, Austria

- Introduction
  - Use of clamping rings / Dynamic issue
- CAE Process
- Validation (1<sup>st</sup> Task)
  - Correlation of testing and simulation / Quasi-static pull-out test
  - Numerical effects using LS-DYNA Explicit for a pull-out test
- Design Parameter (2<sup>nd</sup> Task)
  - Influence of different design parameters of the clamping ring
- High Dynamic Load (3<sup>rd</sup> Task)
  - Impeller burst of a turbo engine / Different failure scenarios
- Summary

### www.inprosim.de

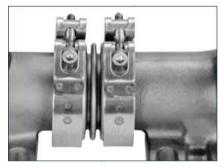
## Introduction

7<sup>th</sup> European LS-DYNA Conference

14th - 15th May 2009, Salzburg, Austria

- Use of clamping rings
  - Connection of two or more parts at the cylindrical flanges
- Examples of common application
  - Several kinds of tubes and pipes or pressure vessels and tanks
- Application in turbo engines
  - Connection of the compressor, turbine and bearing casing of smaller turbo chargers and turbo pumps



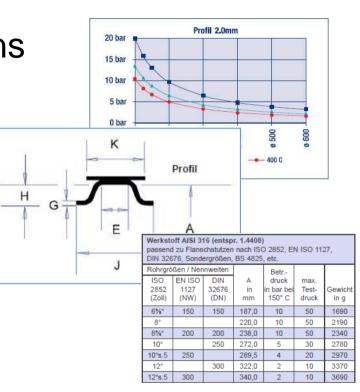




## Introduction

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

- Design for normal operating conditions
  - Standard rules and supplier guide lines
  - Simple static analyses
- Design for highly dynamic loading due to misuse or failure
  - E.g. shock waves, compressor surge, impeller burst
  - Consideration of the effects of the highly dynamic loading (impulse transmitted, mass inertia, non-linear material behaviour, complex contact situation)
  - This can be done using an explicit code like LS-DYNA



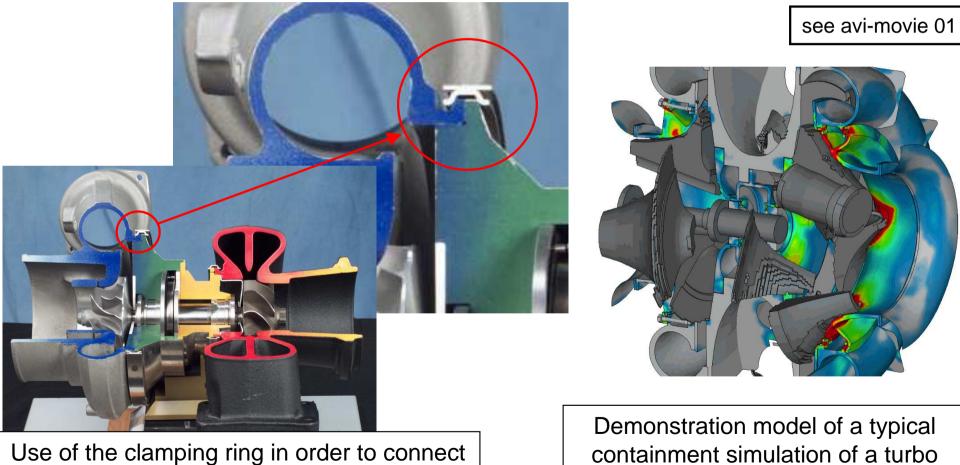
# Introduction

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

charger with highly dynamic loading

### 14<sup>th</sup> May 2009

• Examples: Use of clamping rings in turbo engines



the compressor and bearing casing

# CAE Process

7<sup>th</sup> European LS-DYNA Conference

14th - 15th May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

- Aim
  - Designing a clamping ring for the worst-case scenario of an impeller burst of a small turbo charger
  - The connection of the compressor and bearing casing by the ring must be ensured even for such a highly dynamic loading

## CAE process

- 3 steps lead to a reliable design
- 1<sup>st</sup> task: a <u>quasi-static pull-out test</u> to validate the CAE technique
- 2<sup>nd</sup> task: a <u>parameter analysis</u> of the clamping ring (optionally for better knowledge of essential design parameters)
- 3<sup>nd</sup> task: the <u>burst simulation</u> meaning the highly dynamic loading

14th - 15th May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

## Introduction

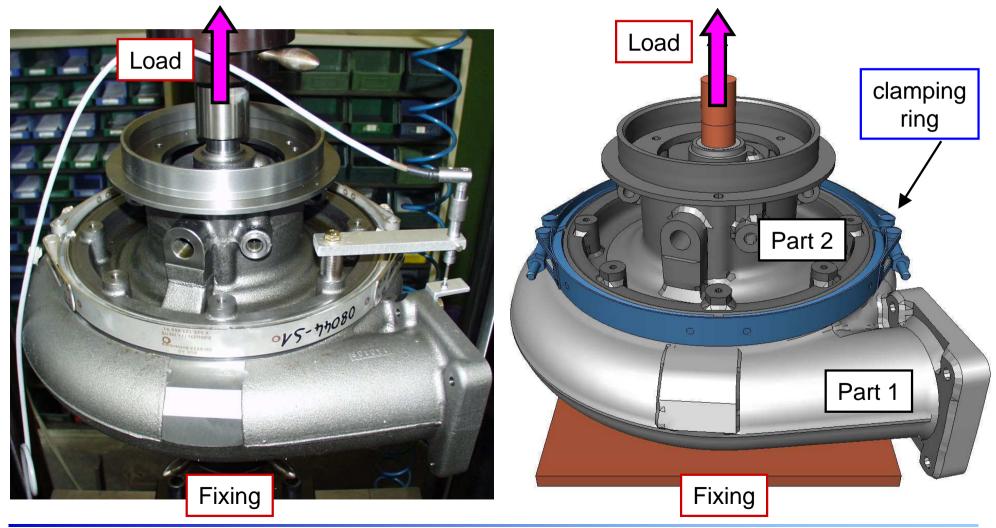
- The 1<sup>st</sup> task in the CAE process is a simulation of a <u>quasi-static</u> <u>pull-out test</u> in order to validate the CAE technique
- A quasi-static pull-out test with real hardware turbo charger parts was carried out as a basis for this validation
- The focus of the validation is on the matching of the load-versusdeflection-curve and the maximum static load capacity
- CAE technique
  - Comparison of the test rig in trial and in simulation
  - Modelling of the pre-stressing of the clamping ring
  - Quasi-static pull-out test in simulation (LS-DYNA Explicit)

7<sup>th</sup> European LS-DYNA Conference

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

14<sup>th</sup> May 2009

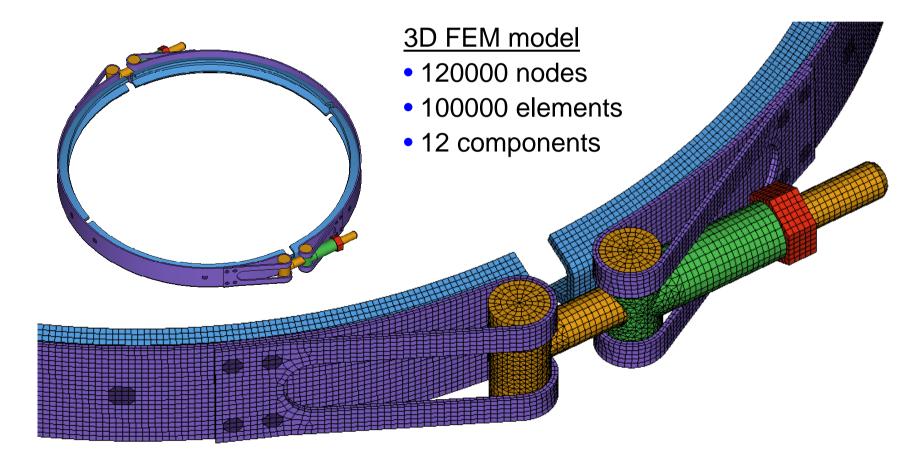
Test ring in trial and in simulation



7<sup>th</sup> European LS-DYNA Conference

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

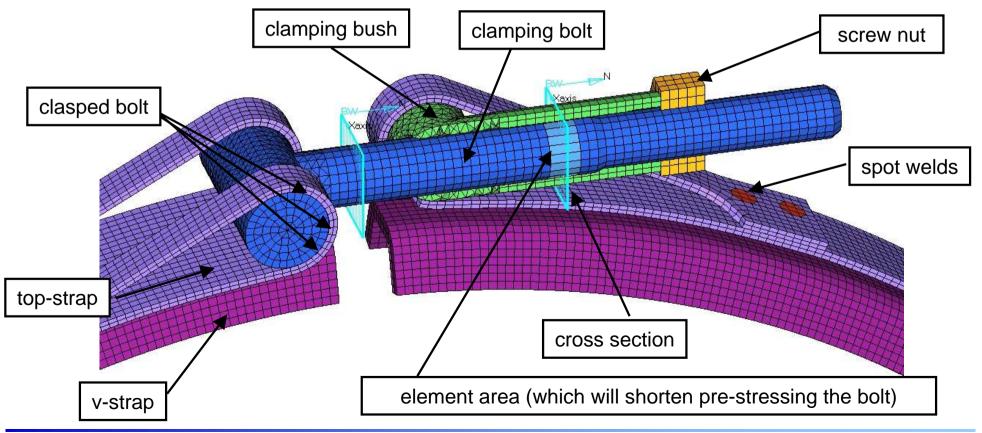
- CAE model technique
  - Typical CAE model of a clamping ring for crash simulation



14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

- CAE technique of the pre-stressed clamping ring
  - 3D model of the clamping ring using brick and tetra elements only

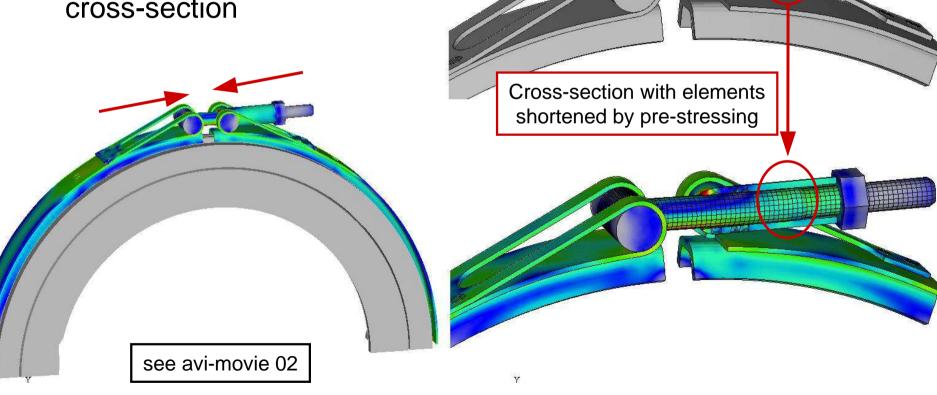


7<sup>th</sup> European LS-DYNA Conference

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

- CAE technique for pre-stressing the clamping ring
  - Pre-stressing of the bolts is realized by shortening the elements at the cross-section

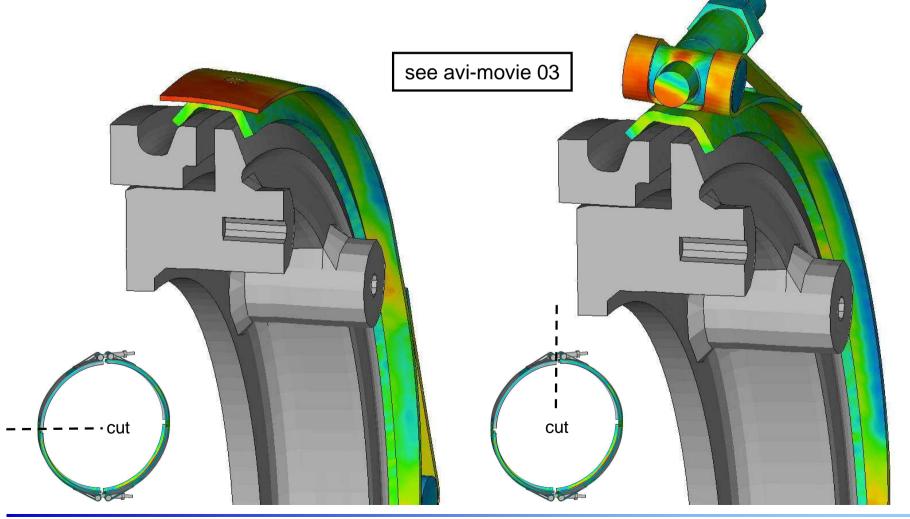


7<sup>th</sup> European LS-DYNA Conference

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

• Quasi-static pull-out test in simulation

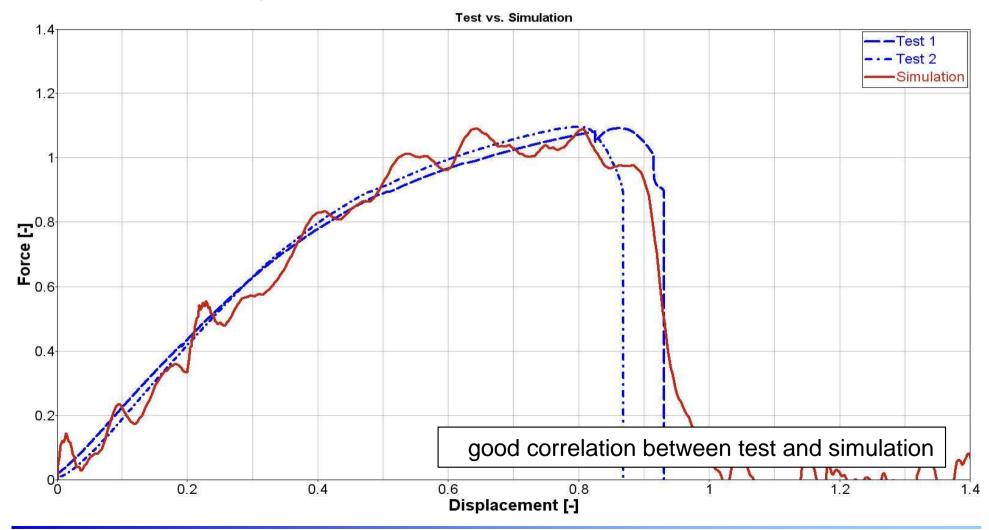


7<sup>th</sup> European LS-DYNA Conference

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

## Quasi-static pull-out test in simulation and trial

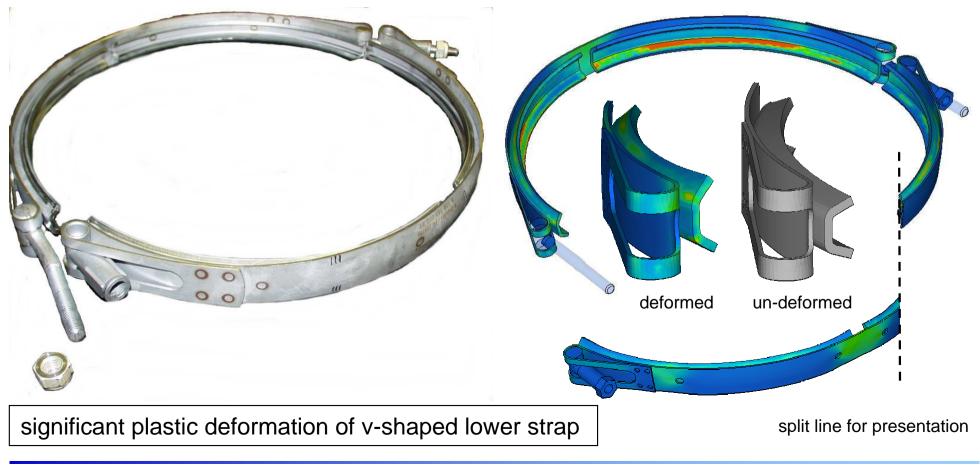


7<sup>th</sup> European LS-DYNA Conference

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

- Quasi-static pull-out test in simulation and trial
  - Good correlation between test and simulation

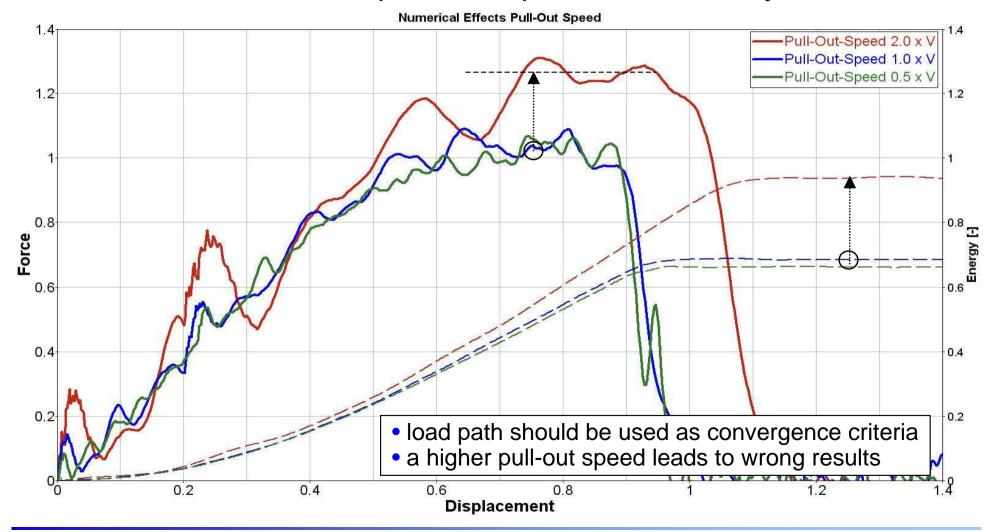


7<sup>th</sup> European LS-DYNA Conference

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

#### 14<sup>th</sup> May 2009

## Use of LS-DYNA Explicit for quasi-static analysis



14th - 15th May 2009, Salzburg, Austria

14<sup>th</sup> May 2009

## Introduction

- The 2<sup>nd</sup> CAE task is a <u>parameter analysis</u> of the clamping ring for getting a better knowledge of the essential design parameters
- This task is optionally, and shown here in order to demonstrate how design issues can be analysed very clearly by simulation

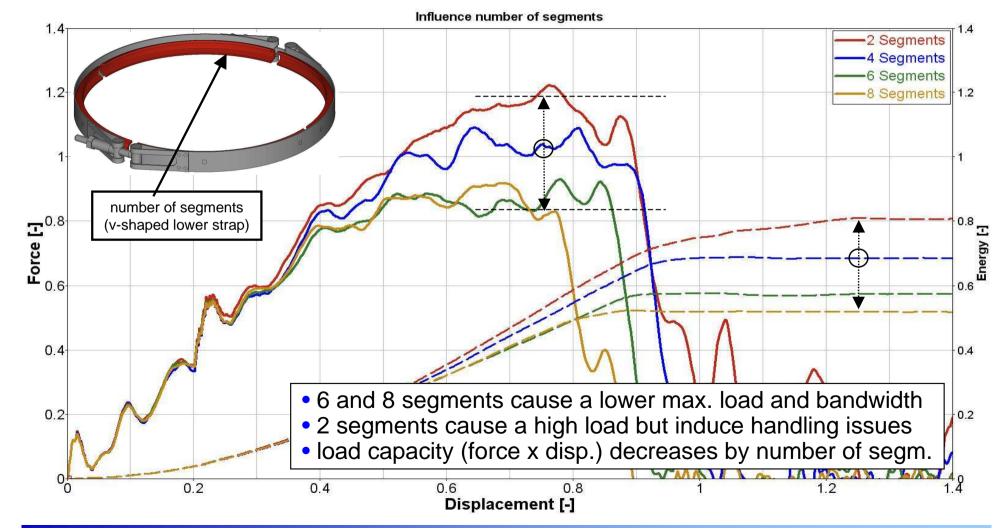
## • Typical design parameters

- The number of the segments of the v-shaped lower strap
- The thickness of the lower v-strap or of the top strap
- The number of the bolts
- The material properties / data
- etc ...

14th - 15th May 2009, Salzburg, Austria

#### 14<sup>th</sup> May 2009

## Influence of the <u>number</u> of the segments of the <u>lower strap</u>



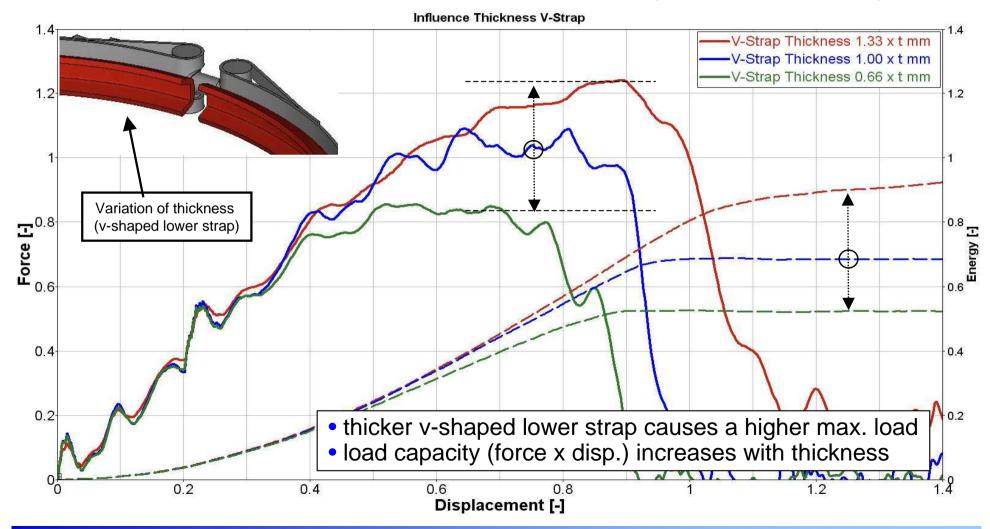
## Parameters

7<sup>th</sup> European LS-DYNA Conference

14th - 15th May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

## Influence of the <u>thickness</u> of the v-shaped <u>lower strap</u>

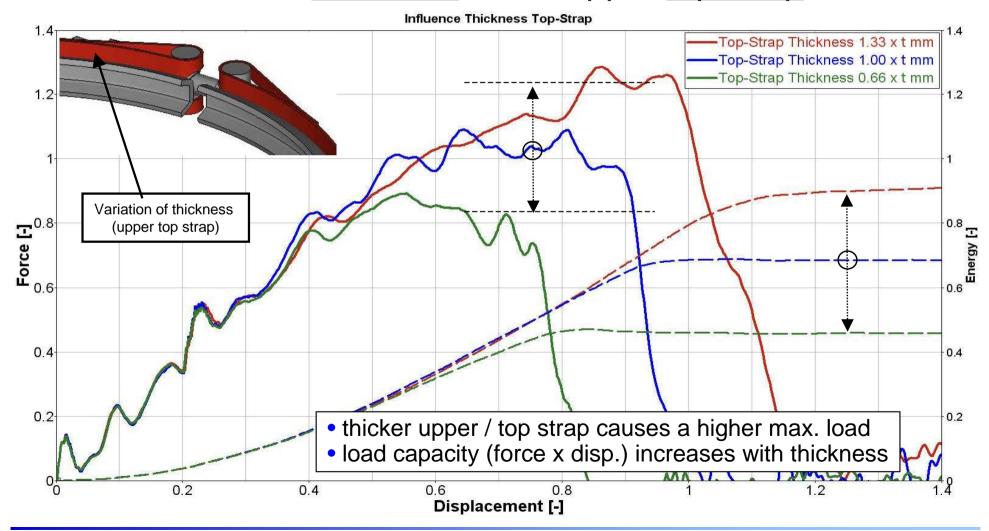




14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

#### 14<sup>th</sup> May 2009

## Influence of the <u>thickness</u> of the upper <u>top strap</u>



# Dynamic load

7<sup>th</sup> European LS-DYNA Conference

14th - 15th May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

## Introduction

- The 3<sup>rd</sup> CAE task is the <u>burst simulation</u> of an impeller burst of a turbo charger with its highly dynamic loading of the clamping ring
- Non-linear material behaviour, dynamic strain rate effects, high rate of plastification with failure, high geometric deformation and the complex contact situation have to be taken into account
- Due to the validation done with the quasi-static pull-out test, the CAE model is reliable for crash simulation purposes too
- CAE technique
  - Using the presented CAE model for explicit analyses
  - Comparison of the forces in dynamic vs. static load case
  - Stiffness balance of the clamping ring and the structure

Dynamic load

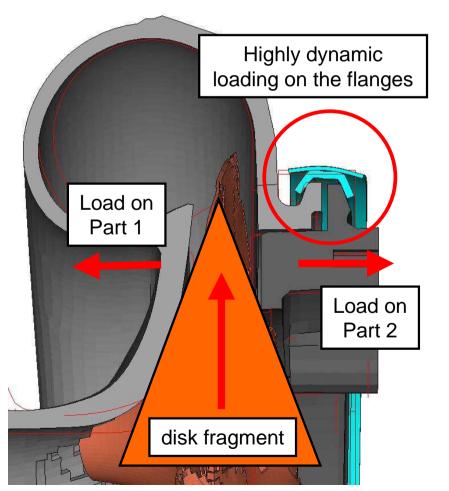
## 7<sup>th</sup> European LS-DYNA Conference

14th - 15th May 2009, Salzburg, Austria

## 14<sup>th</sup> May 2009

## • Containment load case due to the impeller burst

- Failure of the impeller (compressor wheel) releases a high amount of energy and impact load
- The disk fragments move radially entering the airflow channel towards the casing spiral
- Acting like wedges, they introduce a high bending moment and a high axial load into the structure
- In consequence, a highly dynamic loading is applied onto the flanges connecting the compressor and bearing casing

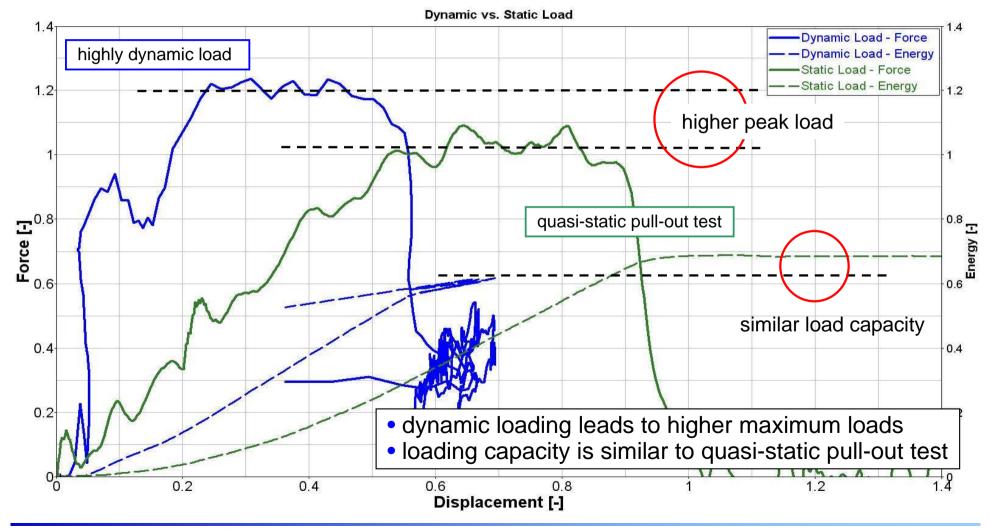




14th - 15th May 2009, Salzburg, Austria

#### 14<sup>th</sup> May 2009

## Clamping ring under high dynamic loading



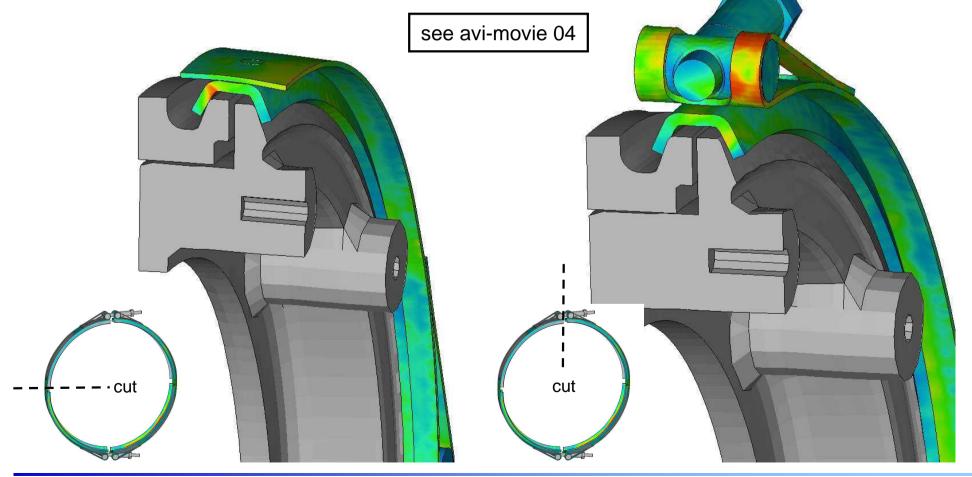
# Dynamic load

7<sup>th</sup> European LS-DYNA Conference

14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

- Clamping ring under highly dynamic loading
  - Good balance of clamping ring and flange structure



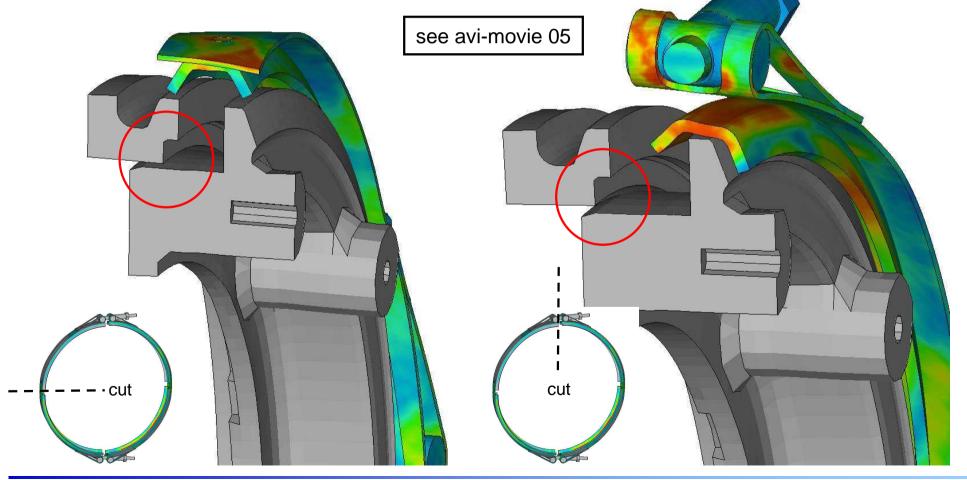


14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

14<sup>th</sup> May 2009

## • Example of a stiffness mismatch

• The clamping ring is too weak, the flange connection is lost



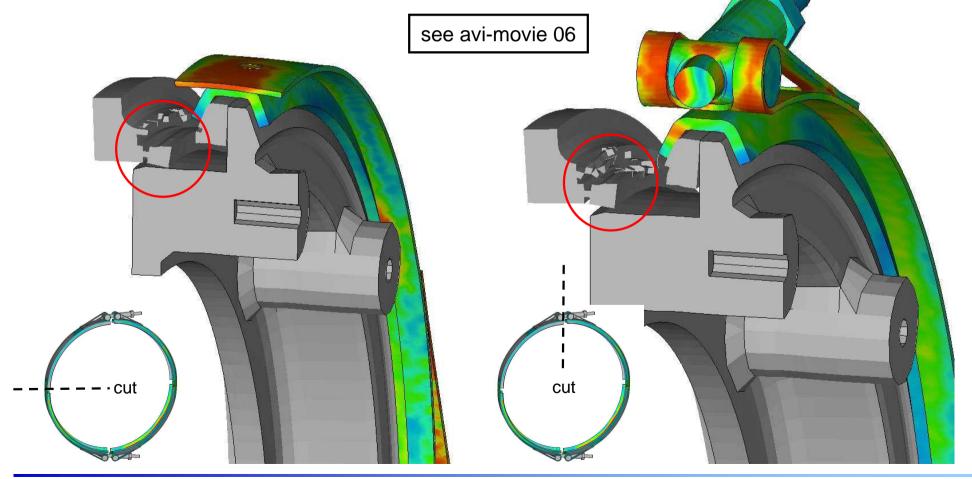


14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

14<sup>th</sup> May 2009

## • Example of a stiffness mismatch

• The clamping ring is too stiff, the flange fails, the connection is lost





14th - 15th May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

## Clamping ring design

- For the worst-case scenario of an impeller burst, standard rules and static analyses for clamping ring design are no longer sufficient
- The highly dynamic loading and non-linear effects in deformation, material behaviour and contact have to be taken into account

## CAE Simulation / Process

- LS-DYNA Explicit is a very efficient tool for designing and optimising a clamping ring under highly loading, as well as for quasi-static simulations like the pull-out test shown
- A validation of a quasi-static pull-out test was carried out in order to improve the reliability of the simulation prediction
- The potential of the CAE optimisation was shown by a parameter study for quasi-static and highly dynamic loading



14<sup>th</sup> - 15<sup>th</sup> May 2009, Salzburg, Austria

### 14<sup>th</sup> May 2009

- Acknowledgment
  - Many thanks to MTU Friedrichshafen GmbH
    - for the kind permission for using the pull-out test results
    - for the excellent teamwork with Dr. B. Koch and Dr. M. Vesper, Engineering Mechanics & Materials



- For any further information, please visit our booth
- or get in contact
  via internet
  www.inprosim.de

